(303) 466-3573



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Environmental Technologies Group ROCKY FLATS SOLARPOND/PONDCRETE PROJECT 452 BURBANK STREET EG&G BUILDING 025 BROOMFIELD, COLORADO 80020

March 2, 1992

Mr. Don Ferrier  $\sqrt[4]{}$ Project Manager
EG&G Rocky Flats, Inc.
5932 McIntyre Street
Golden, Colorado 80403

Subject: Design Criteria for Ponds 207A, B, & C

[WBS 431 PONDSLUDGE PROCESS TRAIN - DESIGN CRITERIA

HALLIBURTON NUS ROCKY FLATS DENVER]

RF-HED-92-0095

Dear Mr. Ferrier:

Enclosed for your approval is the design criteria basis currently being used to design both the 207 A/B and 207C Process Trains. Based on conversations with yourself and Steve Heiman on January 23, 1992 we are submitting these documents for your approval.

The design criterias have been approved by Don Brenneman of HNUS. These incorporate chemical information from the Waste Characterization Report and also geotechnical information which will be incorporated in the next revision of the report. Scheduled for submission prior to March 17, 1992.

Certain criteria for each process train incorporates processing options which HNUS is recommending which should be carefully reviewed by EG&G. These are discussed below and are segregated by each process train.

For the 207A & B processing, the A & B Series Ponds will be consolidated to make a homogenized sludge from the four ponds. The pond sludge will be dewatered at a rate of 4TPH of output filter cake. This information has been included in the inquiry document for the dewatering of the sludges to six subcontractors. This rate will generate an anticipated 6.5 TPH of final waste form. This is substantially less than was discussed in meetings in late January. HNUS recommends this rate to minimize the amount (and expense) of dewatering equipment required to mobilize to site. This processing rate should allow the A & B Series Ponds to be processed in a 45 day period on a two shift/day, 6 days/week basis.

For the 207C Pond and Clarifier processing, one waste stream for cementing will be produced consisting of a 5:1:1 ratio of water, crystals, and silt solids by weight. All treatability study and equipment design is being centered about this ratio. For this processing ratio to occur, the water level within 207C Pond must be brought back to levels observed during the sampling effort on August 22, 1991. This level was 26 inches of total material within the pond. C pond sample will be slurried using these proportions for waste formulation and treatability studies. A separate formula will be developed for a 100% water waste loading to address the final cleanup operation and solidification of final residues. The design criteria indicates that the Clarifier contents will be combined with the 207C Pond prior to waste processing. This will reduce the number of separate processing streams to be tested prior to processing. Currently the treatability study does not incorporate this as a requirement and will need to be incorporated if directed by EG&G.

A-0U04-000362

EG&G Rocky Flats, Inc. Attention: Mr. Don Ferrier Page 2

The current design criteria does not contain any oxidation step to remove cyanide from the Clarifier and C Pond waters. We had a conference call with Ernie Lombardi and Rich Ninesteel today to discuss that issue. Minutes of that conference call will be transmitted under separate cover for your comment. If HNUS must remove cyanide from the waters, substantial schedule impact will occur. We consider this the most critical technical issue to resolve at this time.

We request that you provide approval or comments to the design criteria by March 9, 1992. The flow sheets which were presented to you in a preliminary condition last week are being finalized this week for equipment design and final engineering design. Any changes to the design criteria after that point will have detrimental effects on the schedule.

If you have any questions, please advise.

Sincerely,

HALLIBURTON NUS ENVIRONMENTAL CORPORATION

Ted A. Bittner Project Manager

TAB/jg

Enclosure

cc: S. Heiman (w/o Attachments)

J. Zak

D. Brenneman

R. Ninesteel

A:\LTR\FERRIER-41 RF-HED-92-0095

Original Signed by:

D. R. Brenneman, Vice President

Halliburton NUS Environmental Corporation
February 24, 1992

ISSUE A 2/24/92

		PONDS 207A AND 207B
1.0	GENERA	L
	1.0.1	Processing Rate Product Target Mean 9.6* TPH Range 3.1 - 14.0 TPH
		Feed Target Mean 2.0 TPH dry solids Range 1.0 - 3.1 TPH dry solids
		Percent Solids - Consolidated Ponds  Weighted Average 14.68 No dilution  Reclaimed Range 5 - 158 Estimated  Median Feed 10.08 With dilution
		Filter Cake Percent Solids - Recessed Chamber Average Dry Filter Cake 50% dry solids Range Dry Filter Cake 30 - 65% dry solids
		*Note: Design capacity based on use of one 8" $\phi$ Teledyne Readco mixer as cement mixer. Maximum rate (@ 14.0 TPH) is limited by recessed chamber filter and casting system capacity
	1.0.2	Reclaim/Dewatering System Operating Schedule
		Intermittent Batch Continuous X  2 Shifts/Day  10 Hours/Shift (Overlapping)  6 Days/Week  67 Percent Operating Availability  12 Hours Net Operating Hours/Day
	1.0.3	Cementing Operating Schedule
		Intermittent Batch Continuous X  2 Shifts/Day 10 Hours/Shift (Overlapping) 6 Days/Week 67 Percent Operating Availability 12 Hours Net Operating Hours/Day

Note: NA = Not AnalyzedND = Not Detected

\_\_\_\_ = Data Not Available

# 1.1 POND SLUDGE CHARACTERISTICS - POND 207A

1.1.1	Cumulative Size Distributi	on (U.S. Standard Mesh) (1)
		0.7 %     +3/8"       2.5 %     +4 m (4.75mm)       8.9 %     +10 m (2mm)       29.5 %     +100 m (147μ)       34.7 %     +200 m (74μ)       56.5 %     +400 m (38μ)       43.5 %     -400 m (-38μ)
1.1.2	Specific Gravity	1.011 Liquid (8,9) 1.063 Sludge (8) 1.482 Est. Solids (10)
1.1.3	Estimated Volume (cubic y Contract Scope of Work	ards) 130
	Weston Report	<u>572</u> Liquid <sub>TOTAL</sub> (12) <u>4.2</u> Sludge (12)
	JHT - 2/14/92	300 Liquid (13) 30 Sludge (13)
1.1.4	Sludge Terminal Density	12.7% % Solids (8) 11.2-12.7% % Solids (6,8)
1.1.5	Sludge Moisture (Grav.) (Karl Fisher)	87.3-88.8% % Liquid (8) 34 % Liquid (9)
1.1.6	pH - Liquid - Sludge	9.79 (9) 8.9 (9)
1.1.7	Specific Conductance	9000 μmho/cm Liquid (9)
1.1.8	Total Dissolved Solids	7.800 gpl (9)
1.1.9	Predominant Cations (Liquid)	Ca (0.0715 gpl) (5) Mg (0.0918 gpl) K (0.2560 gpl) Na (1.0300 qpl)
	(Liquid)	Ca (ND) (9)  Mg (0.123 gpl)  K (0.394 gpl)  Na (1.860 gpl)

	1.1.9	(Sludge)	Mg (11,400 mg/kg) (9)  K (ND)  Na (14,500 mg/kg)  Cr ( 658 mg/kg)  Cd ( 1,300 mg/kg)
	1.1.10	Predominant Anions (Liquid)	Cl (0.400 gpl) (9) CN - Total 0.43 ppm
•		(Sludge)	TOC (14,000 mg/kg) (9)
	1.1.11	Sludge Viscosity	NA
	1.1.12	Sludge Liquid Limit	NA
	1.1.13	Sludge Plastic Index	NA
	1.1.14	Sludge Plastic Limit	NA
1.2		UDGE CHARACTERISTICS - Cumulative Size Distrik	oution (U.S. Standard Mesh) (1) $ \begin{array}{ccccccccccccccccccccccccccccccccccc$
		(Reference 8)	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
	1.2.2	Specific Gravity	1.008 Liquid (8,9) 1.175 Sludge (8) 1.682 Est. Solids (10)

1.2.3	Estimated Volume (cubic y Contract Scope of Work	ards)
	Weston Report	4,803 Liquid <sub>TOTAL</sub> (12) 659 Sludge (12)
	JHT - 2/14/92	2,980 Liquid (13) 820 Sludge (13)
1.2.4	Sludge Terminal Density	24.9% % Solids (8) 23.2-28.2% % Solids (6,8)
1.2.5	Sludge Moisture (Grav.) (Karl Fisher)	71.8-76.8% % Liquid (8) 25.6% % Liquid (9)
1.2.6	pH - Liquid - Sludge	<u>8.4</u> (9)
1.2.7	Specific Conductance	NA Liquid
1.2.8	Total Dissolved Solids	<u>2.800 gpl</u> (9)
1.2.9	Predominant Cations (Liquid)	Ca (0.138 gpl) (9)  Mg (0.065 gpl)  K (0.056 gpl)  Na (0.296 gpl)
	(Sludge)	Mg ( 3,805 mg/kg) (9)  Na (ND)  K (ND)  Cr ( 23.2 mg/kg)  Cd ( 7.1 mg/kg)
1.2.10	Predominant Anions (Liquid)	Chloride (98 ppm) (9) CN-Total (0.03 ppm)
	(Sludge)	TOC (3,200 mg/kg) (9)
1.2.11	Sludge Viscosity	NA NA
1.2.12	Sludge Liquid Limit	72.8* (8,9)
1.2.13	Sludge Plastic Index	37.3* (8,9)
1.2.14	Sludge Plastic Limit	35.5* (8,9)

\* Untreated

# 1.3 POND SLUDGE CHARACTERISTICS - POND 207B CENTER

1.3.1	Cumulative Size Distribut:	ion (1) $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
1.3.2	Specific Gravity	1.017 Liquid (8,9) 1.045 Sludge (8) 1.348 Est. Solids (10)
1.3.3	Estimated Volume (cubic year) Contract Scope of Work	ards)
	Weston Report	3,631 Liquid <sub>TOTAL</sub> (12) 766 Sludge (12)
	JHT - 2/14/92	780 Liquid (13) 820 Sludge (13)
1.3.4	Sludge Terminal Density	8.7% % Solids (8) 6.6-10.1% % Solids (6,8)
1.3.5	Sludge Moisture (Grav.) (Karl Fisher)	89.9-93.4% % Liquid (8) 48.3% % Liquid (9)
1.3.6	pH - Liquid - Sludge	9.1 9.2 (9)
1.3.7	Specific Conductance	14,500 μmhos/cm Liquid(9)
1.3.8	Total Dissolved Solids	16.00 gpl (9)
1.3.9	Predominant Cations (Liquid)	Ca (0.027 gpl) (9) Mg (0.218 gpl) K (0.800 gpl) Na (3.150 gpl)
	(Sludge)	Mg (12,400 mg/kg) (9)  K (10,700 mg/kg)  Na (42,000 mg/kg)  Cr (63.1 mg/kg)  Cd (57.9 mg/kg)

	1.3.10	Predominant Anions (Liquid)	Chloride ND (9) CN-Total (0.64) ppm
		(Sludge)	TOC (7,400 mg/kg) (9)
	1.3.11	Sludge Viscosity	NA
	1.3.12	Sludge Liquid Limit	82.8* (8,9)
	1.3.13	Sludge Plastic Index	<u>28.5*</u> (8,9)
	1.3.14	Sludge Plastic Limit	52.3* (8,9)
		* Untreated	
1.4	POND S	LUDGE CHARACTERISTICS - PON	ND 207B SOUTH
	1.4.1	Cumulative Size Distributi	on (1)
		1	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
	1.4.2	Specific Gravity	1.019       Liquid       (8,9)         1.065       Sludge       (8)         1.466       Est. Solids       (10)
	1.4.3	Estimated Volume (cubic ya Contract Scope of Work	rds)
		Weston Report	3,611 Liquid <sub>TOTAL</sub> (12) 786 Sludge (12)
		JHT - 2/12/92	4,715 Liquid (13) 820 Sludge (13)
	1.4.4	Sludge Terminal Density	10.4% % Solids (8) 7.9-11.7% % Solids (6,8)
	1.4.5	Sludge Moisture (Grav.) (Karl Fisher)	88.3-92.1% % Liquid (8) 45.3% % Liquid (9)

	1.4.6	pH - Liquid - Sludge	9.07	(9)
	1.4.7	Specific Conductance	17,300 μmhos/cm Liq	uid ( <del>9</del> )
	1.4.8	Total Dissolved Solids	14.50 gpl	(9)
	1.4.9	Predominant Cations (Liquid)	Ca (0.052 gpl) Mg (0.188 gpl) K (0.691 gpl) Na (2.360 gpl)	(9)
		(Sludge)	Mg (10,500 mg/kg) Na (30,000 mg/kg) Cr ( 38.1 mg/kg) Cd ( 22.8 mg/kg)	(9)
	1.4.10	Predominant Anions (Liquid)	Chloride ND CN-Total (1.3 ppm)	(9)
		(Sludge)	TOC (8,600 mg/kg)	_ (9)
	1.4.11	Sludge Viscosity	NA NA	
	1.4.12	Sludge Liquid Limit	NA	
	1.4.13	Sludge Plastic Index	NA	
	1.4.14	Sludge Plastic Limit	NA NA	
1.5		LUDGE CHARACTERISTICS - COM Led Average Values)	BINED 207A & 207B P	ONDS (10)
	1.5.1	Cumulative Size Distributi	on 0.2 % +3/8"	(1)
		_	0.6 % +4 m (4 3.4 % +10 m 16.7 % +100 m 21.9 % +200 m 39.0 % +400 m 61.0 % -400 m	(2mm) (147μ) (74μ)
	1.5.2	Specific Gravity	1.015 Liquid 1.100 Sludge 1.569 Est. Solids	(8,9) (8) (10)

1.5.	.3 Estimated Volume (cubic Contract Scope of Work	2,375 Liquid (2) 2,375 Sludge (11)
	Weston Report	12,618 Liquid <sub>TOTAL</sub> (12) 2,215 Sludge (12)
	JHT - 2/14/92	8,775 Liquid (13) 2,490 Sludge (13)
1.5	.4 Sludge Terminal Density	14.6% % Solids (8) 6.6-28.2% % Solids (6,8)
1.5	.5 Sludge Moisture (Grav.) (Karl Fisher)	71.8-93.4% % Liquid (8) 39.4% % Liquid (10)
1.5	.6 Sludge Viscosity	NA
(Not	D RECLAIM SYSTEM te: Sub-contractor Scop delines for interfacing w cessing.)	pe. Criteria provided as ith downstream stabilization
1.6	.1 Maximum Particle Size l	Reclaimed 1-12 inch
1.6	.2 Nominal Reclaim Rate	100 - 400 gpm
1.6	.3 Particle Size Cut Point	in Scalping Screen 10 mesh
1.6	.4 Responsibility For Pond	d Oversize Removal <u>EG&amp;G</u>
1.6	.5 Responsibility For Pond	d Cleaning <u>EG&amp;G</u>
1.6	.6 Responsibility For Scr	een Oversize <u>EG&amp;G</u>
1.6	.7 Reclaim System To Be	X Leased Purchased
1.6	.8 Reclaim System Type R	esponsibility of Sub-Contr.
1.6	.9 Estimated Reclaim Slur	ry Density <u>10 % Solids</u>
1.6	.10 Estimated Sludge Speci: (For Estimated Average	fic Gravity $\frac{1.065}{\text{Solids S.G.}}$

### 1.7 SIZE LIMITATION

(Note: Sub-contractor Scope. Criteria provided as guidelines for interfacing with downstream stabilization processing.)

1.7.1 Particle Size Requirements to Cementing Operation

100% Passing 10 U.S. mesh or 2000 microns 80% Max. Passing 400 mesh or 38 microns

- 1.7.2 Particle Size Limit To Filtration
  100% Passing 10 U.S. mesh or 0.078 inch
- 1.7.3 Oversize From Screen Scalping \_\_\_\_\_ To half crate box
- 1.8 POND CONSOLIDATION/GRAVITY SETTLING (Note: Sub-contractor Scope)

Calcium Hypochlorite For L/S Separation Improvement and Pathogenic Treatment 201bs/ton\* dry solids in feed

\*Note: @ 10% solids in feed, 20 lbs/ton dry solids is equivalent to 1000 ppm of 65% calcium hypochlorite added to slurry (2.0 lbs/ton slurry). This is consistent with maintaining a minimum of 2.0 ppm free chlorine for 30 minutes.

1.8.2 Flocculant Type Very High Charge Cationic
Polyacrylamide by Stockhausen & CIE
PRAESTOL 644BC or equivalent

\*Note: Flocculant listed is typical, included as an example only.

- 1.8.3 Flocculant Dosage 10-20 lbs/ton solids @ 0.1% Soln.
- 1.8.4 Sludge Consolidated in 207B South Pond\*

\*Note: Additions made to initial 207C pond contents by reclaim and circulation prior to consolidation and addition of contents of other ponds.

1.8.5 Decant Consolidated in 207B North Pond

1.9 DEWATE	RING PRESSURE	FILTER
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(Note: Sub-contractor Scope. Criteria provided as guidelines for interfacing with downstream stabilization processing. Assumptions based on utilization of recessed chamber or diaphragm pressure filter.)

1.9.1 Pressure Filter Feed Rate

(GPM feed @ 10% solids) Nominal: 165 gpm Range: 145 - 185 qpm 1.9.2 Filter Cake Nominal: 60.0 % Solids Range: 40 - 65 % Solids 1.9.3 Design Basis 2.0 lbs dry solids/hr/ft2 (@ 60% solids cake)  $1.0 - 3.0 \, lbs/hr/ft^2$ Range: Flocculant Used X YES NO 1.9.4 (Coagulant) 1.9.5 Flocculant Type High Charge Cationic Quaternary (Coagulant) <u> Amine - American Cyanamid's</u> Magnafloc<sup>TM</sup> 581C\*

\*Note: Flocculant listed is typical, included as an example only.

- 1.9.6 Flocculant Dosage 15 lbs/ton solids @ 10% Solution (Coagulant)
- 1.9.7 Lime (Hydrated) Added Prior To Filtration (Optional)

\*Note: All lime required for stabilization mix may be added prior to filtration to improve filtration rate and soften filtrate. Based on 8.0% lime added to total stabilized waste minus available lime in flyash (equivalent to 5.18% of flyash weight), additional lime which would be added in cementing:

30% Solids Filter Cake 1,055 lbs lime/ton solids 50% Solids Filter Cake \_\_\_546 lbs lime/ton solids 60% Solids Filter Cake 419 lbs lime/ton solids

1.9.7 Cake Discharge/Surge Hopper Residence Time

2 hours product (@ 50% solids) (≈200 cubic foot capacity)

	1.9.8	Size Of Broken Cake	Nominal 1" X 2" or Smaller (Suitable for conveyor transport)
	1.9.9	Filter Cycle Time	One cycle/filter every two hours based on two ≈90 cubic foot capacity filter.
1.10	CEMENT	ING AND CASTING	
	1.10.1	Feed Holding/Surge Re	esidence Time 2 hours product (@ 50% solids) (~200 cubic foot capacity)
	1.10.2	Feed Surge Mixer (Ble	ender) Residence Time Nominal 20 minutes ( @ 50% solids filter cake - ≈ 57 cubic foot capacity)
	1.10.3	Cement Mixer Type	Low-Residence-Time, High- Intensity Continuous Mixer (e.g. Teledyne Readco 8"\$\phi\$)
	1.10.4	pH Requirements	10.5-11.5 Precementing 12.2+ Cementing
	1.10.5	pH Adjusted With	Hydrated Lime Note: 8.0 wt.% net Lime added to Stabilized Mix (see Section 1.9.7) in blender (surge hopper).
·	1.10.6	Other Additives Precementing Surge Hopper	Viscosity Modifier (Optional) Fly Ash Type C

1.10.7	Cementing Stabilizat (Treating dry solids solids cake, Range:	as aggregate, Target Feed	(14) l: 50%
	Pond Liquid	0.5 PARTS 21.2%	Mean
	Pond Solids (DRY)	1.0-0.35 35.0-100% 0.5 PARTS 21.2%	Range Mean
	Cement TYPE V	0.0-0.65 0.0-65.0% 0.40 PARTS 16.8%	Range Mean
	Fly Ash TYPE C	0.28-0.79 14.0-22.0% 0.80 PARTS 33.7%	Range Mean
	Total Hydrated Lime	0.17 PARTS 7.1%	Range Mean Range
	*Note: Based on Free	Water/(Cement+Flyash) = 0	.42
1.10.8	Other Characteristics	s of Cement Waste Form	
	Slump (inches) Cast in ½ Crates If NO, How?	0-1 YES X Pellet or Briquette deposited in half	NO
	Pressure Pumpable?	YESX	NO
	Strength (psi)  @Time =  Method  Maximum Temperature  Other Pass pair	600+ Target28	days
		·84 Paint Can Test	
		lon containers sample per	
	<u>waste for</u>	m batch.	
1.10.9	Casting System Requir - Product discharge move container.	ements must be interruptable to	<b></b>
		pellets or extrusions.	_ _
		ty packing in container.	_
	- Needs casting weig		_
	<pre>documents to accom - Final certification</pre>		-
		II WEIGHT DY EGAG.	

1.11	FORTDMI	ENT LOCATION
1.11	ngorem	ENI LOCATION
	1.11.1	Pond Consolidation System
		Located on West side of 207B South between
		207A pond and 207B ponds.
	1.11.2	Pond Reclaim System
	•	Located within pond berm area and on West side
		of 207B South between 207A pond and 207B
		ponds. Pump to size limitation and
		pretreatment (chlorination and polymer
		addition) before dewatering or during pond
		consolidation.
	1.11.3	Size Limitation and Pretreatment
		Located on West side of 207B South between
		207A pond and 207B ponds.
	1.11.4	Dewatering
		Located South of 207A and SW of 207B ponds.
	1 11 5	O-mantinu
	1.11.5	Cementing
		Located South of 207A and SW of 207B ponds.
		Product of mixer discharges into pelletizer
		or briquetter prior to casting station.
	1 11 6	Casting
	1.11.0	Enclosed structure with HEPA filtration
		system capable of supporting 14.0 tph product.
		System capable of supporting 14.0 cpm produce.
1.12	OTHER C	CONSIDERATIONS
		Prior to transport to 750 pad, container lid
		must be set on half crate container, fiber-
		glass cover set over container lid and
		composite container secured with strapping.
		- Demposite Confedition Design with Betapping.
		Cementing equipment to be relocated to 904
		pad for use with Pondcrete/Saltcrete. Thus,
		capacity of all feeders and equipment capable
		of handling 14.0 tph maximum product rate.

#### 2.0 REFERENCES

- (1) Based on Weston Memo, M. E. Selman to T. Bittner, July 16, 1991, Excerpts From Pond Sludge Sampling Report, Issued July, 1991
- (2) <u>Statement of Work, Solar Ponds and Pondcrete</u>, April 16, 1991 (Revision: October 14, 1991)
- (3) Assumption as per D. R. Brenneman, Halliburton NUS Environmental Corporation
- (4) Weston Health & Safety Plan, <u>Sampling Solar Pond</u>
  <u>Water</u>, <u>Sludge</u>, <u>and Sediment</u>, <u>April 1991</u>
- (5) NUS <u>Draft Waste Sampling Plan</u>, Received June 5. 1991)
- (6) Weston, <u>Pond Sludge Sampling Report</u>, Issued, July, 1991
- (7) HNUS Pittsburgh, Technical Memo, <u>Treatability</u>
  <u>Testing Performed at Halliburton NUS Laboratory</u>,
  <u>Pittsburgh</u>, <u>Pennsylvania</u>, December, 1991
- (8) Memo of Pond Sludge Characterization Data, November 14, 1991, HNUS, Pittsburgh
- (9) HNUS Pittsburgh, <u>Pond Sludge and Clarifier Sludge</u>
  <u>Waste Characterization Report, Deliverables 224A and</u>
  <u>224E Combined</u>, Draft Issued January, 1992
- (10) B&R Houston IOM, <u>Suggested Pond 207A&B Composite Mix</u>
  Ratios, January 10, 1992
- (11) HNUS, <u>Special Conditions Report, Revision 3</u>, November 7, 1991
- (12) <u>Table 2: Estimated Quantities From Weston Report</u>
  <u>Data</u>, Pond Sludge Design Basis Memo, August 26, 1991
- (13) Amendment I, February 12, 1992, Request For Proposal

   Stage 1 Densification, Subcontractor Scope Of
  Work, Attachment 2 (By JHT, 2/12/92)
- (14) HNUS FAX, SM to TB, February 21, 1992, Stabilization Mix Recipes Second Cut

Signed:

Original Signed By:

D. R. Brenneman, Vice President

Halliburton NUS Environmental Corporation

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Date:

Original Signed by:

D. R. Brenneman, Vice President

Halliburton NUS Environmental Corporation
February 24, 1992

ISSUE A 2/24/92

# PROCESS DESIGN CRITERIA PONDS 207C AND CLARIFIER SLUDGE

#### 1.0 GENERAL

1.0.1 Processing Rate

Product

Target Mean <u>14.0\*</u> TPH
Range <u>7.0 - 18.5</u> TPH

Feed

TPH drv\*\* solids (22)

Target Mean 0.985 TPH dry\*\* solids Range 0.00 - 2.28 TPH dry\*\* solids

Percent Solids 16.2% Median 0.0 - 32.0% Range

Total Rate 6.23 STPH Slurry Feed 17.0 GPM Slurry Flow

\*Note: Design capacity based on one  $8"\phi$  Teledyne Readco mixer.

\*\*Note: Assumption is that pond 207C level maintained at 26" depth consistent with condition of pond on August 22, 1991 (Reference 20: JHT to WCH, February 21, 1992). This is equivalent to pond slope linear measurement of 185" at reference point. This gives approximate volume ratio of brine:salt:silt of 5:1:1 which has resulted in a successful stabilized waste form (cement/flyash/lime) (Reference 21: SM to TB, 2/21/94). The 207C pond consists of dry salt crystals and inert solids, dry basis.

Note: NA = Not Analyzed

ND = Not Detected

\_\_\_\_ = Data Not Available

1.0.2	Pond 207C Physical Materia (Note: Based on Reference	
	Salt Crystals Percent of Pond Feed Water of Hydration Dry Salt	
	Silt (Settled Sludge Sludge Sludge Sludge) Percent of Pond Feed Inert Solids Liquid (Water+Salt)	
	Pond Liquid Phase (Bring Percent of Pond Feed Water Salt (Dissolved)	
	Free Water In Pond Solid Salt In Pond TDS Salt In Pond Silt Inerts In Pond	45.3% Weight % 6.7% Weight % 38.6% Weight % 9.4% Weight %
1.0.3	Reclaim/Milling System Ope	erating Schedule
	2 Shifts/Day10 Hours/Shift6 Days/Week67 Percent Open	Continuous X  (Overlapping)  rating Availability Operating Hours/Day
1.0.4	Cementing Operating Schedu	ıle
	6 Days/Week	(Overlapping)
		rating Availability Operating Hours/Day

# 1.1

POND S	LUDGE CHARACTERIS	STICS - PO	ND 207C
1.1.1	Cumulative Size	Distributi	on (U.S. Standard Mesh) (1)
	Salt Crystals Or	nly	13.2 % +3/8"  48.1 % +4 m (4.75mm)  89.8 % +10 m (2mm)  99.1 % +100 m (147μ)  99.1 % +200 m (74μ)  99.1 % +400 m (38μ)  0.9 % -400 m (-38μ)
1.1.2	Specific Gravity		1.332 Liquid (8,9) 316 - 1.348 Range 1.613 Sludge (30%) (12) 2.256 Dry Salt* (12) 2.077 Hydr. Salt* (12)
	*Note: Crystall 16.6% water base	ine salt ed on EG&G	(dry) assumed to contain Building 374 data.
	Recent data for Total Water Total Dry S Slurry S.G.	: Salt	1" (16)  58.2% Weight % Liquid  41.8% Weight % Solids  1.43
	Calculated S.G.	Salt	2.029 Using water (17) 1.566 Using brine (17)
	Recent data for Total Water Total Dry S Slurry S.G.	alt	lids" (16)  40.8% Weight % Liquid  59.2% Weight % Solids  1.46
	Calculated S.G.	Salt	1.777 Using water (17) 1.548 Using brine (17)
1.1.3	Est. Current Vol Contract Scope of		yards)
	Weston Report		916 Liquid (13) 956 Sludge (13)
	JHT - 2/14/92		
	JHT - 8/22/91	≈5.0 ≈1.0 ≈1.0	1,551 Liquid (20)  314 Silt Slurry (20)  322 Salt Crystals (20)

1.1.4	Sludge Terminal Density (In Lab Sample of Salt)	60.5% % Solids 51.6 - 65.2% % Solids	(8) (8)
1.1.5	Sludge Moisture (Karl Fisher)	NA % Liquid	(9)
1.1.6	pH - Liquid - Sludge	10.08 10.47	(8)
1.1.7	Specific Conductance (Liquid)	>50,000 μmho/cm 51,000 μmho/cm	(9) (18)
1.1.8	Total Dissolved Solids	460.0 qpl 300-510 qpl Range	(9)
		400.0 gpl	(6)
1.1.9	Predominant Cations (Liquid)	Ca (>0.200 qpl) B (0.3600 qpl) K (78.700 qpl) Na (102.00 qpl)	(6)
	(Liquid)	Ca (ND) B (0.463 qpl) K (5.580 %) Na (13.80 %)	(9)
	(Sludge)	Mg (3,370 mg/kg) Na(157,600 mg/kg) Cr (618 mg/kg) Cd (164 mg/kg)	(9)
1.1.10	Predominant Anions (Liquid)	Cl (0.023 gpl) CN-Total(7.7 ppm)	(9)
	(Sludge)	Cl NA CN-Total (72 ppm) TOC (7,700 mg/kg)	(9)
1.1.11	Sludge Viscosity	NA	
1.1.12	Sludge Liquid Limit	NA	
1.1.13	Sludge Plastic Index	NA NA	
1.1.14	Sludge Plastic Limit	NA	

# 1.2 CLARIFIER SLUDGE CHARACTERISTICS\*

(\*Note: Assumption is that clarifier sludge and liquid will be introduced into 207C as a slurry pond prior to processing.)

1.2.1 Cumulative Size Distribution (U.S. Standard Mesh)

		,
		* +3/8"  * +4 m (4.75mm)  * +10 m (2mm)  * +100 m (147μ)  * +200 m (74μ)  * +400 m (38μ)  * -400 m (-38μ)
1.2.2	Specific Gravity	Liquid Sludge Est. Solids
1.2.3	Est. Current Volume (Gallons)	20,000 Liquid (3) 5,000 Sludge
1.2.4	Sludge Terminal Density	39.4 % Solids (9) 27.5-66.9 % Solids (9)
1.2.5	Sludge Moisture (Grav.) (Karl Fisher)	% Liquid % Free Liquid
1.2.6	pH - Liquid - Sludge	<u>10.0</u> (9)
1.2.7	Specific Conductance (Liquid)	$34,500 \ \mu \text{mho/cm} \qquad (9)$
1.2.8	Total Dissolved Solids	59.00 gpl (9)
1.2.9	Predominant Cations (Liquid)	Ca (ND) (9)  Mg (0.004 gpl)  K (0.057 gpl)  Na (0.012 gpl)  B (0.028 gpl)
	(Sludge)	Mg (20,500 mg/kg) (9)  Na (78,000 mg/kg)  K (56,900 mg/kg)  Cr (2,480 mg/kg)  Cd (3,660 mg/kg)  Ni (700 mg/kg)  Ag (135 mg/kg)  CN Total 87 ppm

1.2.10	Predominant Anions (Liquid)		2.09 gpl) L (2.7 ppm)	(9)
	(Sludge)	TOC (5,1	75 mg/kg)	<del>(9</del> )
1.2.11	Sludge Viscosity	<del> </del>		
1.2.12	Sludge Liquid Limit			
1.2.13	Sludge Plastic Index	•	·	
1.2.14	Sludge Plastic Limit			
1.3 207C PG	OND RECLAIM SYSTEM			
1.3.1	Maximum Particle Size	Reclaimed	2.0	inch
1.3.2	Nominal Reclaim Rate		100 - 400	_ gpm
1.3.3	Nominal Brine Slurry Processing Rate	14	.9 gpm	(15) ::
1.3.4	Responsibility For Po	nd Oversize Re	moval <u>EG&amp;</u>	G
1.3.5	Responsibility For Po	ond Cleaning	EG8	G
1.3.6	Reclaim System To Be		eased urchased	
1.3.7		Hydraulic adjusted ratio of solid conform to treat results (Pond of 8/22/91). Vacuum-assist pumping system	ds to liquid eatability state 207C condition	to cudy ions
1.3.8	Estimated Reclaim Slu	rry Density Range:	16.2% Sc 0-20% Sc	lids olids
1.3.9	Estimated Sludge Spec (For Solids S.G. = 2.		1.613	

C - 3

1	. 4	DOND	2070	CTTD	REDUCTION	r
	- 4	PUND	2070	SIZE	- REDUCTED ON	1

1.4.1 Particle Size Requirements to Cementing Operation

100% Passing 10 U.S. mesh or 2000 microns 80% Max. Passing 400 mesh or 38 microns

- 1.4.2 Particle Size Limit To Pin Mill 100% Passing 1½ inch
- 1.4.3 Additions Prior To Transport\* Hydrated Lime to pH = 10.5 11.0Estimated  $\approx 20$  lbs/ton slurry @16.2% solids

Calcium Hypochlorite for Pathogenic Treatment

20 lbs/ton slurry

\*Note: @16.2% Net dry solids in feed brine slurry, 20 lb/ton slurry of 65% calcium hypochlorite is equivalent to 1000 ppm added to slurry. This is consistent with sustaining a minimum 2.0 ppm free chlorine residual in solution after 30 minutes. Equipment required for calcium hypochlorite addition to be leased from reclaim system operator.

## 1.5 CLARIFIER SLUDGE RECLAIM SYSTEM

1.5.1 Reclaim System Type

Vacuum-Assisted Pump\* and

Existing Diaphraqm U/F pumps
used to transfer clarifier
sludge to 207C pond to
commingle for processing.

\*Note: Leased unit

### 1.6 CEMENTING AND CASTING

- 1.6.1 Feed Holding or Surge Capacity \_\_\_\_\_\_ 30 \_\_\_\_ Minutes Minimum at 14 TPH Product Rate
- 1.6.2 Cement Mixer Type

  Low-Residence-Time, HighIntensity Continuous Mixer
  (e.g. 8"\$\phi\$ Teledyne Readco)
- 1.6.3 pH Requirements 10.5-11.5 Precementing 12.2+ Cementing
- 1.6.4 pH Adjusted With Hydrated Lime

1.6.5	Other Additives	
	Precementing	None (FeSO, optional)
	-	Hydrated Lime added @ 8% of
		stabilization mix weight -
		·
	Brine treatment of	only: 0.141 tons lime/ton soln.
	Pond Level of 8/2	22/91: 0.137 tons lime/ton slurry
	Pond Level of 11	13/91: 0.139 tons lime/ton slurry
	Cementing	<u> Viscosity Modifier (Optional)</u>
	-	Fly Ash Type C (S.G. = $2.74$ )
		Cement Type V (S.G. = 3.17)
		See below
1.6.6	Cementing Stabili:	zation Parameters - Pond 207C (21)
	(Note: Free Wate	r/(Cement+Flyash) = 0.420)
	•	
	Target Mid-Point:	Pond Condition of 8/22/91 (20)
	Target Low:	Brine only
	Target High:	Pond Condition of 11/13/91 (20)
	Pond Liquid	0.680 PARTS 30.3% Mean
		0.30-1.00 PARTS 14.7-40.7% Range
	Pond Salt Mush	0.160 PARTS 7.1% Mean
		0.00-0.20 PARTS 0.0- 9.8% Range
	Pond Silt Slurry	
		0.00-0.51 PARTS 0.0-25.0% Range
	Cement TYPE V	0.358 PARTS 16.0% Mean
		0.29-0.43 PARTS 14.3-17.4% Range
	Fly Ash Type C	0.718 PARTS 32.0% Mean
		0.58-0.86 PARTS 28.5-34.9% Range
	Hydrated Lime	0.167 PARTS 7.4% Mean
	(Total)	0.16-0.17 PARTS 6.9-8.4% Range
	(2002)	
1.6.7	Cementing Stabili	zation Parameters - Clarifier (20)
1.0.,	(Note: The assum	otion is that clarifier sludge will
	be combined and m	ixed with 207C contents. At 25,000
	gallone versus 45	50,000+ gallons in 207C pond, the
	miv would contain	slightly over 5% of the clarifier
	sludge; thus wou	ald have the properties of 207C
	alone.)	ite itera and brahararas as acto
	alone.	

1	6 9	Other	Characteristics	of	Cement	Waste	Form
1 .	n . x	Orner	Characteristics	O.L	Cement	masce	101

Slump Cast in ½ Crates If NO, How? Pressure Pumpable? Hardness (psig) @Time = Method Maximum Temperature Other Pass paint fi	X YES	NO  et  28 days UCS
	container sampl	e per
waste form ba		
1.6.9 Casting System Requirement  - Recipe is envisioned to  - Special splash protect needs to be integrated  - Initial set time estime  - Other criteria similare  - Needs casting weight and to accompany waste for  - Final certification we  - Shroud over half crated during pouring to impress	ts o be a liquid. ion during pour into the desig ated to be 30 m to ponds A&B. nd operating do m. ight by EG&G. may be require	n. inutes. cuments
1.6.10 Holding Station		
<ul> <li>Needs to hold filled h</li> </ul>	alf crates for	30
minutes to set suffici		
- Moved to 750 pad for c	<u>uring after ins</u>	<u>pection</u>
and initial set.		

# 1.7 EQUIPMENT LOCATION

1.7.1 Pond Reclaim System

- Located within or adjacent to pond berm area at
SW end of 207C pond.

- Includes pump to size reduction (Pin Mill) and
before transport to pretreatment and cementing.

1.7.2 Size Reduction

- Delumper, overflow head tank and pin mill are
located South or SW of 207C pond.

- Transport pipeline from pin mill sump to first
pretreatment tank located South of 207A pond.

# 1.7.3 Pretreatment

- First pretreatment tank where calcium hypochlorite and FeSO, (if needed) are added is a
  gravity-overflow agitated tank (one of two in series). It is located South of 207A pond and
  also serves as receiving/surge tank.

   The second pretreatment tank is where the lime
  for pH adjustment and additional lime required
  for the stabilization mix is added. It is added
  as a solid powder and is mixed in the tank. The
  tank is pumped from the bottom and circulated.
- Slurry feed to the cementing is controlled on the recycle stream.

# 1.7.4 Cementing

- Located South of 207A and SW of 207B ponds.
- Product of mixer discharges into half crates in casting station.

# 1.7.5 Casting

 Located South of 207A pond at end of cementing train.

### 1.8 OTHER CONSIDERATIONS

- Same as those for A&B train except that most of this equipment (possibly the FeSO, and calcium hypochlorite systems and surge tanks) will not be used on the 904 pad.

## 2.0 REFERENCES

- (1) Based on Weston Memo, M. E. Selman to T. Bittner, July 16, 1991, Excerpts From Pond Sludge Sampling Report, Issued July, 1991
- (2) <u>Statement of Work, Solar Ponds and Pondcrete</u>, April 16, 1991 (Revision: October 14, 1991)
- (3) Assumption as per DRB, H/NUSEC
- (4) Weston Health & Safety Plan, <u>Sampling Solar Pond</u>
  <u>Water</u>, <u>Sludge</u>, <u>and Sediment</u>, <u>April 1991</u>
- (5) NUS <u>Draft Waste Sampling Plan</u>, Received June 5. 1991)
- (6) Weston, <u>Pond Sludge Sampling Report</u>, Issued, July, 1991
- (7) HNUS Pittsburgh, Technical Memo, <u>Treatability</u>
  <u>Testing Performed at Halliburton NUS Laboratory</u>,
  <u>Pittsburgh</u>, <u>Pennsylvania</u>, <u>December</u>, 1991
- (8) Memo of Pond Sludge Characterization Data, November 14, 1991, HNUS, Pittsburgh
- (9) HNUS Pittsburgh, <u>Pond Sludge and Clarifier Sludge</u>
  <u>Waste Characterization Report, Deliverables 224A and</u>
  <u>224E Combined</u>, Draft Issued January, 1992
- (10) B&R Houston IOM, <u>Suggested Pond 207A&B Composite Mix</u>
  Ratios, January 10, 1992
- (11) HNUS, <u>Special Conditions Report</u>, <u>Revision 3</u>, November 7, 1991
- (12) Table 6a: Process Inputs to Pure Salt Processing (POND 207C), Saltcrete DBM, November 11, 1991, Revision a, 1/27/92
- (13) Table 2: Estimated Quantities From Weston Report

  Data, Pond Sludge DBM, August 26, 1991, (Based on
  information supplied to TB by JG, EG&G, June 1991
  and pond volume calculations by JHT, July 1991)
- (14) HNUS Memo, SM to DRB, January 29, 1992, <u>Preliminary</u>
  <u>Design Information</u>

- (15) B&R Memo, WCH to JRZ, February 6, 1992, Material Balances For Pond Sludge Processing Revision 5a, Plan B For Ponds 207A&B and Plan C For Pond 207C And Clarifier Using Mix Formulations and Assumptions of Memo: SM to DRB, 1/29/92, (i.e. Reference 14)
- (16) HNUS, FAX RMN to TB, February 12, 1992, 207C Starting Mix Calculation
- (17) B&R Memo, WCH to JRZ, February 17, 1992, Interpretations Of Recent Mixture Data Supplied By HNUS (RMN to TB, 2/12/92)
- (18) HNUS Memo, SM to DRB, February 10, 1992, Treatability Studies Status Report (Week of Feb. 3-7, 1992)
- (19) Amendment I, February 12, 1992, Request For Proposal

   Stage 1 Densification, Subcontractor Scope Of
  Work, Attachment 2 (By JHT, 2/12/92)
- (20) B&R Memo, JHT to WCH, February 21, 1992, Volume of Solids and Solution in the 207C Pond
- (21) HNUS FAX, SM to TB, February 21, 1992, Stabilization Mix Recipes Second Cut
- (22) B&R Memo, WCH to JRZ, February 24, 1992, <u>Material Balance Revision 6 Equivalent Material Balances for 207A&B and 207C Pond & Clarifier For Design Criteria, Issue 0</u>

Signed:	Original Signed By:  D. R. Brenneman, Vice President Halliburton NUS Environmental Corporation
Date:	2/24/92